## Amendments to the Claims:

The listing of claims will replace all prior versions, and listing, of claims in the application:

## Listing of Claims:

(currently amended): A method for <u>in-phase and quadrature</u> #Q mismatch calibration of a transmitter, comprising the following steps:

generating a discrete-time signal  $x[n] = x(n \cdot T_s)$ , wherein  $x(t) = e^{j2\pi f_1 t}$  and  $f_T$  and  $T_s$  are real numbers:

obtaining a corrected signal  $x_c[n]$  based on the signal x[n] and a set of correction parameters  $A_p$  and  $B_p$ , wherein  $x_c[n] = A_p \cdot x[n] + B_p \cdot x^*[n]$ ;

converting the corrected signal  $x_c[n]$  to an analog corrected signal  $x_c(t)$ ; applying <u>in-phase and quadrature #Q-modulation</u> to the analog corrected signal  $x_o(t)$  and outputting a modulated signal  $x_o(t)$ :

- obtaining a first desired component measure  $W^{(1)}(f_T)$  and a first image component measure  $W^{(1)}(-f_T)$  from the modulated signal  $x_m(t)$  with a first set of the correction parameters  $A_0$  and  $B_0$ :
- obtaining a second desired component measure  $W^{(2)}(f_T)$  and a second image component measure  $W^{(2)}(-f_T)$  from the modulated signal  $x_m(t)$  with a second set of the correction parameters  $A_0$  and  $B_0$ :

- obtaining a third desired component measure  $W^{(3)}(f_T)$  and a third image component measure  $W^{(3)}(-f_T)$  from the modulated signal  $x_m(t)$  with a third set of the correction parameters  $A_p$  and  $B_p$ ;
- obtaining a fourth and fifth set of correction parameters  $A_p$  and  $B_p$  based on the first, the second, and the third desired component measures as well as the first, the second, and the third image component measures;
- obtaining a fourth desired component measure  $W^{(4)}(f_T)$  and a fourth image component measure  $W^{(4)}(-f_T)$  from the modulated signal  $x_m(t)$  with the fourth set of correction parameters  $A_p$  and  $B_p$ ;
- obtaining a fifth desired component measure  $W^{(5)}(f_T)$  and a fifth image component measure  $W^{(5)}(-f_T)$  from the modulated signal  $x_m(t)$  with the fifth set of correction parameters  $A_\rho$  and  $B_\rho$ ; and
- obtaining a final set of the correction parameters  $A_p$  and  $B_p$  from the fourth and fifth sets of correction parameters.
- 2. (currently amended): The method for <u>in-phase and quadrature  $\mbox{$\mathbb{H}$}\mbox{$\mathbb{Q}$}$  mismatch calibration of a transmitter as claimed in claim 1, wherein the first set of correction parameters  $(A_p,B_p)=(a,0)$ , the second set of correction parameters  $(A_p,B_p)=(b,b)$ , and the third set of correction parameters  $(A_p,B_p)=(b,-b)$ , where a and b are real numbers.</u>

- 3. (currently amended): The method for <u>in-phase and quadrature  $\frac{1}{2}$  wherein the parameter a is 1 and the parameter b is  $\frac{1}{2}$ .</u>
- 4. (currently amended): The method for <u>in-phase and quadrature </u>#Q mismatch calibration of a transmitter as claimed in claim 1, wherein the fourth set of correction parameters (*A<sub>p</sub>*,*B<sub>p</sub>*) are obtained by

$$A_{p} = \sqrt{P} - j\hat{\alpha}\sqrt{Q}$$

$$B_{p} = -\hat{\alpha}\sqrt{P} - j\sqrt{Q}$$

and the fifth set of correction parameters  $(A_p,B_p)$  are obtained by

$$A_{p} = \sqrt{P} + j\hat{\alpha}\sqrt{Q}$$

$$B_{p} = -\hat{\alpha}\sqrt{P} + j\sqrt{Q}$$

where

$$\alpha \approx \hat{\alpha} = \frac{\sqrt{N_O} - 1}{\sqrt{N_O} + 1},$$

$$N = (W^{(2)}(f_T) + W^{(2)}(-f_T))/2,$$

$$O = (W^{(3)}(f_T) + W^{(3)}(-f_T))/2,$$

$$Q = \frac{\hat{\alpha}^2 - \rho^{(1)}}{(1 + \rho^{(1)})(\hat{\alpha}^2 - 1)},$$

$$P = 1 - Q,$$

$$\rho^{(1)} = \frac{W^{(1)}(-f_T)}{W^{(1)}(f_T)}.$$

- 5. (currently amended): The method for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 1, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(-f_T)$  is less than the function of  $W^{(5)}(-f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.
- 6. (currently amended): The method for <u>in-phase and quadrature WQ mismatch calibration</u> of a transmitter as claimed in claim 5, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if <u>a value of  $W^{(4)}(-f_T)$ </u> is less than <u>a value of  $W^{(5)}(-f_T)$ </u>, otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.
- 7. (currently amended): The method for <u>in-phase and quadrature VQ</u> mismatch calibration of a transmitter as claimed in claim 1, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(f_T)$  is greater than the function of  $W^{(5)}(f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.
- (currently amended): The method for <u>in-phase and quadrature </u>#Q
   mismatch calibration of a transmitter as claimed in claim 7, wherein the final set

of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if <u>a value of</u>  $W^{(4)}(f_r)$  is greater than <u>a value of</u>  $W^{(5)}(f_r)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

9. (currently amended): The method for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 1, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(-f_T)$  and  $W^{(4)}(f_T)$  is less than the function of  $W^{(5)}(-f_T)$  and  $W^{(5)}(-f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

10. (currently amended): The method for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 9, wherein the final set of correction parameters  $(A_p, B_p)$  is set to be the fourth set of correction parameters if  $W^{(4)}(-f_T)/W^{(4)}(f_T)$  is less than  $W^{(5)}(-f_T)/W^{(5)}(f_T)$ , otherwise the final set of correction parameters  $(A_p, B_p)$  is set to be the fifth set of correction parameters.

11. (currently amended): The method for in-phase and quadrature I/Q mismatch calibration of a transmitter as claimed in claim 1, further comprising the following steps:

- further adding <u>a</u> an-DC compensation parameter  $\gamma_p$  while obtaining the corrected signal  $x_c[n]$  such that  $x_c[n] = A_p \cdot (x[n] + \gamma_p) + B_p \cdot (x[n] + \gamma_p)^* \; ;$
- obtaining a first local leakage component measure  $L_1$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $\gamma_p = \zeta_1$ , where  $\zeta_1$  is a real number;
- obtaining a second local leakage component measure  $L_2$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_{p_1}$  and the parameter  $\gamma_c = \zeta_2$ , where  $\zeta_2$  is a real number;
- obtaining a third local leakage component measure  $L_3$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $y_n = i\zeta_1$ ;
- obtaining a fourth local leakage component measure  $L_4$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $y_0 = i\zeta_0$ ;
- obtaining a fifth local leakage component measure  $L_5$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $p_0$ =0; and
- obtaining a final DC compensation parameter  $\gamma_{_{F,fleal}}$  based on the first local leakage component measure  $L_1$ , the second local leakage component measure  $L_2$ , the third local leakage component measure  $L_4$  and the fifth local leakage component measure  $L_5$ .

12. (currently amended):The method for <u>in-phase and quadrature  $\mbox{\it lf}$  with mismatch calibration of a transmitter as claimed in claim 11, wherein the final DC compensation parameter  $\gamma_{p,final}$  is obtained by</u>

$$\gamma_{p,\mathit{final}} = -\frac{1}{2} \cdot \frac{\zeta_2^2(L_1 - L_s) - \zeta_1^2(L_2 - L_s)}{\zeta_1(L_2 - L_s) - \zeta_2(L_1 - L_s)} - j \frac{1}{2} \cdot \frac{\zeta_2^2(L_3 - L_s) - \zeta_1^2(L_4 - L_s)}{\zeta_1(L_4 - L_s) - \zeta_2(L_3 - L_s)}.$$

- 13. (currently amended): An apparatus for <u>in-phase and quadrature </u>#Q mismatch calibration of a transmitter, comprising:
  - a signal generator for generating a discrete-time signal  $x[n] = x(n \cdot T_s)$ , wherein  $x(t) = e^{j2\pi f_s t}$  and  $f_T$  and  $T_S$  are real numbers;
  - a correction module for receiving the discrete-time signal x[n] and obtaining a corrected signal  $x_c[n]$  based on the test-signal x[n] and a set of correction parameters  $A_p$  and  $B_p$ , wherein  $x_c[n] = A_p \cdot x[n] + B_p \cdot x^*[n]$ ;
  - a first and second D/A converter converting the corrected signal  $x_c[n]$  to an analog signal  $x_c(t)$ , wherein the first D/A converter converts the real part of the corrected signal to <u>a</u>\_the-real part of the analog signal, and the second D/A converter converts the imaginary part of the corrected signal to <u>an\_the\_inaginary\_part of the\_inaginary\_part of the\_inaginary\_p</u>
  - a modulator applying <u>in-phase and quadrature VQ-modulation</u> to the analog signal  $x_n(t)$ , and outputting a modulated signal  $x_m(t)$ :

- a measurer configured to for implementing the steps of:
  - obtain obtaining-a first desired component measure  $W^{(i)}(f_T)$  and a first image component measure  $W^{(i)}(-f_T)$  from the modulated signal  $x_m(t)$  with a first set of the correction parameters  $A_0$  and  $B_0$ ;
  - obtain obtaining-a second desired component measure  $W^{(2)}(f_T)$  and a second image component measure  $W^{(2)}(-f_T)$  from the modulated signal  $x_m(t)$  with a second set of the correction parameters  $A_p$  and  $B_p$ ;
  - obtain obtaining a third desired component measure  $W^{(3)}(f_T)$  and a third image component measure  $W^{(3)}(-f_T)$  from the modulated signal  $x_m(t)$  with a third set of the correction parameters  $A_0$  and  $B_0$ ;
  - obtain obtaining—a fourth desired component measure  $W^{(4)}(f_{\tilde{r}})$  and a fourth image component measure  $W^{(4)}(-f_{\tilde{r}})$  from the modulated signal  $x_m(t)$  with a fourth set of correction parameters  $A_n$  and  $B_n$ ; and
  - obtain obtaining-a fifth desired component measure  $W^{(5)}(f_T)$  and a fifth image component measure  $W^{(5)}(-f_T)$  from the modulated signal  $x_m(t)$  with a fifth set of correction parameters  $A_p$  and  $B_p$ ; and

a processor configured to for implementing the steps of:

obtain obtaining-the fourth and fifth sets of correction parameters  $A_p$  and  $B_p$  based on the first, the second, and the third desired component measures as well as the first, the second, and the third image component measures; and  $\frac{\text{choose ehoesing-a final set of correction parameters } A_p \text{ and } B_p$  from the fourth and fifth sets of correction parameters.

- 14. (currently amended): The apparatus for <u>in-phase and quadrature  $\mbox{\sc HQ}$  mismatch calibration of a transmitter as claimed in claim 13, wherein the first set of correction parameters  $(A_p,B_p)=(a,0)$ , the second set of correction parameters  $(A_p,B_p)=(b,b)$ , and the third set of correction parameters  $(A_p,B_p)=(b,b)$ , where a and b are real numbers.</u>
- 15. (currently amended): The apparatus for <u>in-phase and quadrature  $\mbox{$\scalebox{$</u>$
- 16. (currently amended): The apparatus for <u>in-phase and quadrature  $\frac{1}{2}$ </u> mismatch calibration of a transmitter as claimed in claim 13, wherein the fourth set of correction parameters ( $A_n$ ,  $B_0$ ) are obtained by

$$A_{p} = \sqrt{P} - j\hat{\alpha}\sqrt{Q}$$

$$B_{p} = -\hat{\alpha}\sqrt{P} - j\sqrt{Q}$$

and the fifth set of correction parameters  $(A_p,B_p)$  are obtained by

$$A_{p} = \sqrt{P} + j\hat{\alpha}\sqrt{Q}$$

$$B_{p} = -\hat{\alpha}\sqrt{P} + j\sqrt{Q}$$

where

$$\begin{split} \alpha \approx \hat{\alpha} &= \frac{\sqrt{N_O} - 1}{\sqrt{N_O} + 1}, \\ N &= (W^{(2)}(f_T) + W^{(2)}(-f_T))/2, \\ O &= (W^{(3)}(f_T) + W^{(3)}(-f_T))/2, \\ Q &= \frac{\hat{\alpha}^2 - \rho^{(1)}}{(1 + \rho^{(1)})(\hat{\alpha}^2 - 1)}, \\ P &= 1 - Q, \\ \rho^{(1)} &= \frac{W^{(1)}(-f_T)}{W^{(1)}(f_T)}. \end{split}$$

17. (currently amended): The apparatus for <u>in-phase and quadrature  $\Psi Q$ </u> mismatch calibration of a transmitter as claimed in claim 13, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(-f_T)$  is less than the function of  $W^{(5)}(-f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

18. (currently amended): The apparatus for <u>in-phase and quadrature  $\mbox{$\mathbb{I}$}\mbox{$\mathbb{I}$}$  mismatch calibration of a transmitter as claimed in claim 17, wherein the final set of correction parameters  $(A_0,B_0)$  is set to be the fourth set of correction</u>

parameters if <u>a value of</u>  $W^{(4)}(-f_T)$  is less than <u>a value of</u>  $W^{(5)}(-f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

19. (currently amended): The apparatus for <u>in-phase and quadrature  $\Psi$ Q</u> mismatch calibration of a transmitter as claimed in claim 13, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(f_{\bar{r}})$  is greater than the function of  $W^{(5)}(f_{\bar{r}})$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

20. (currently amended): The apparatus for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 19, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if <u>a value of  $W^{(4)}(f_T)$ </u> is greater than <u>a value of  $W^{(5)}(f_T)$ </u>, otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

21. (currently amended): The apparatus for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 13, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if a function of  $W^{(4)}(-f_{\star})$  and  $W^{(4)}(f_{\star})$  is less than the function of

 $W^{(5)}(-f_T)$  and  $W^{(5)}(f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.

- 22. (currently amended): The apparatus for <u>in-phase and quadrature WQ</u> mismatch calibration of a transmitter as claimed in claim 21, wherein the final set of correction parameters  $(A_p,B_p)$  is set to be the fourth set of correction parameters if  $W^{(4)}(-f_T)/W^{(4)}(f_T)$  is less than  $W^{(5)}(-f_T)/W^{(5)}(f_T)$ , otherwise the final set of correction parameters  $(A_p,B_p)$  is set to be the fifth set of correction parameters.
- 23. (currently amended): The apparatus for <u>in-phase and quadrature #Q</u> mismatch calibration of a transmitter as claimed in claim 13, wherein the processor further configured to <u>implementing the steps of</u>:

further add a adding-an-DC compensation parameter  $\gamma_{\mathcal{P}}$  while obtaining the corrected signal  $x_{\mathcal{E}}[n]$  such that  $x_{\mathcal{E}}[n] = A_{x^{-1}}(x[n] + \gamma_{x^{-1}}) + B_{x^{-1}}(x[n] + \gamma_{x^{-1}})^{*};$ 

- obtain obtaining—a first local leakage component measure  $L_1$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_{p_1}$  and the parameter  $\gamma_c = \zeta_1$ , where  $\zeta_1$  is a real number;
- obtain obtaining-a second local leakage component measure  $L_2$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $\gamma_0 = \zeta_2$ , where  $\zeta_2$  is a real number;

- obtain obtaining—a third local leakage component measure  $L_3$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $\gamma_p = j\zeta_1$ ;
- obtain obtaining-a fourth local leakage component measure  $L_4$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_p$ , and the parameter  $\gamma_p = j\zeta_2$ ;
- obtain ebtaining—a fifth local leakage component measure  $L_5$  from the modulated signal  $x_m(t)$  with the final set of parameters  $A_p$  and  $B_{p_1}$  and the parameter  $\gamma_p$  =0; and
- obtain obtaining-a final DC compensation parameter  $\gamma_{p,final}$  based on the first local leakage component measure  $L_1$ , the second local leakage component measure  $L_2$ , the third local leakage component measure  $L_3$ , the fourth local leakage component measure  $L_4$  and the fifth local leakage component measure  $L_5$ .
- 24. (currently amended): The apparatus for <u>in-phase and quadrature  $\mbox{${\it l}$}\mbox{${\it l}$}\m</u>$

$$\gamma_{p,\mathit{final}} = -\frac{1}{2} \cdot \frac{\zeta_2^2(L_1 - L_s) - \zeta_1^2(L_2 - L_s)}{\zeta_1(L_2 - L_s) - \zeta_2(L_1 - L_s)} - j \frac{1}{2} \cdot \frac{\zeta_2^2(L_3 - L_s) - \zeta_1^2(L_4 - L_s)}{\zeta_1(L_4 - L_s) - \zeta_2(L_3 - L_s)}.$$